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Offshore Wind Foundations

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Managing Director– Gavin and Doherty Geosolutions Ltd. (GDG)



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Gavin & Doherty Geosolutions

Gavin & Doherty Geosolutions Ltd. (GDG) is a specialist geotechnical engineering consultancy, providing innovative geotechnical solutions across a broad range of civil engineering sectors. Our geotechnical engineers provide services to both the domestic and international markets including concept design, detailed design, in-situ monitoring and general geotechnical advice.

We moved to a new office! Address:
Unit A2, Nutgrove Office Park
Rathfarnham, Dublin 14, D14 X627

Delivering the most progressive, reliable, and efficient geotechnical designs
across a wide variety of subjects and situations



Infrastructure



Offshore



Structures



Renewables



Research &
Development



➤ LEANWIND Work Package 2

**Construction, Deployment and
Decommissioning**

Work Package Leader: GDG

Main Focus

- Cost and time optimisation/innovation of wind farm life cycle
- Innovative substructure concepts



- Introduction
- Foundation Optimisation
 - XL Monopiles
 - Gravity Base Foundations
- Concept Development
 - Floating Jackets
 - Floating Platform

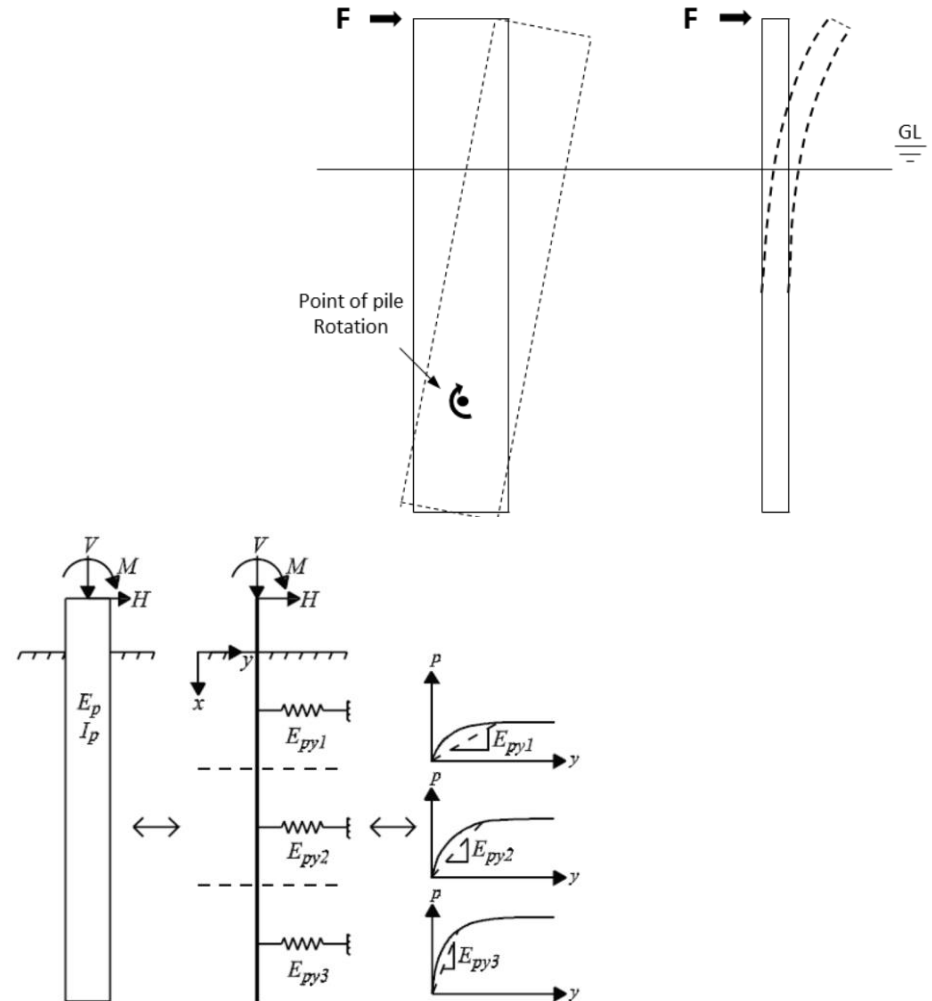


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Traditional Monopile Design

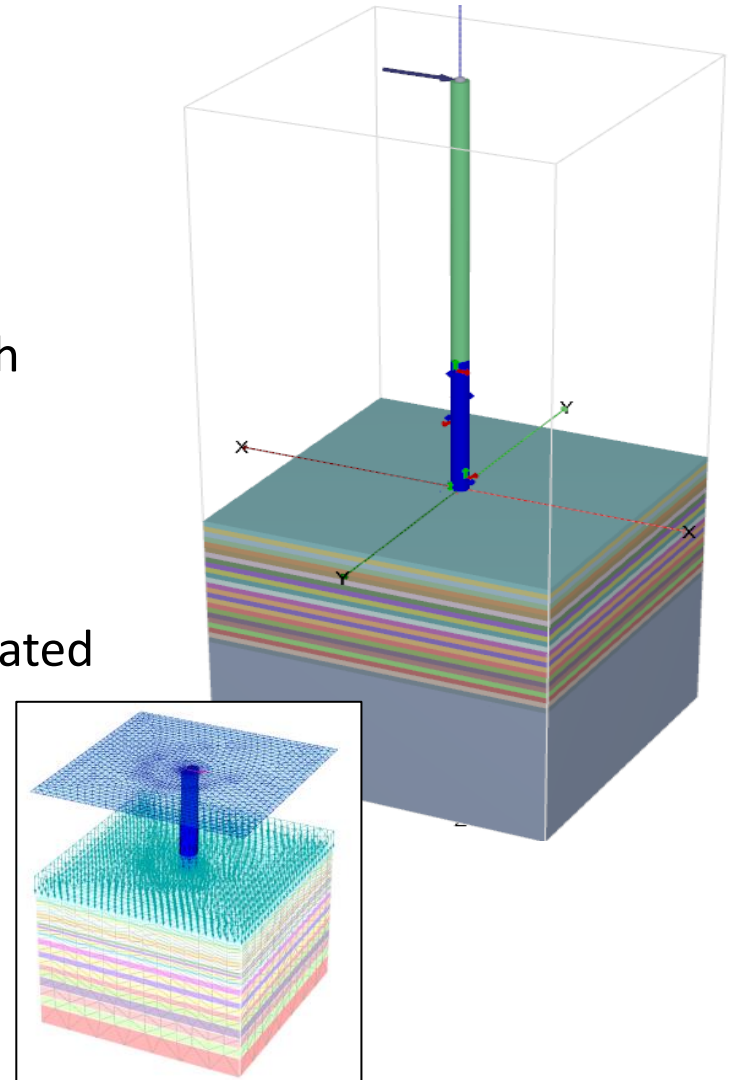
- Lateral Pile Response typically using 1D FE 'p-y' approach
- API 'p-y' curves derived from small diameter (0.6m diameter), slender pile tests – Not suitable for monopiles typically >4m
- API approach thought to be conservative for monopiles
- Implemented in 1D FE model software (Lpile)

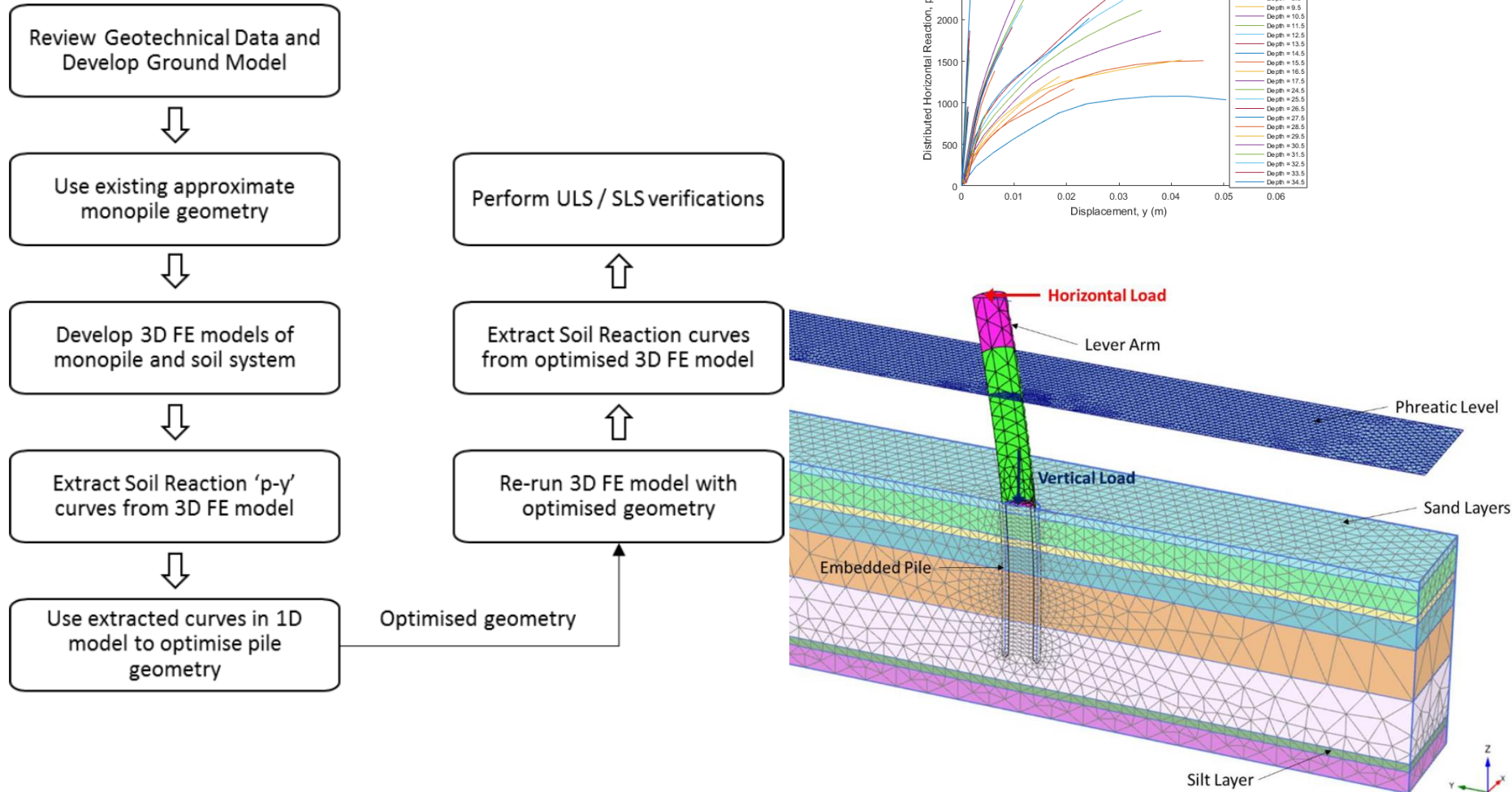


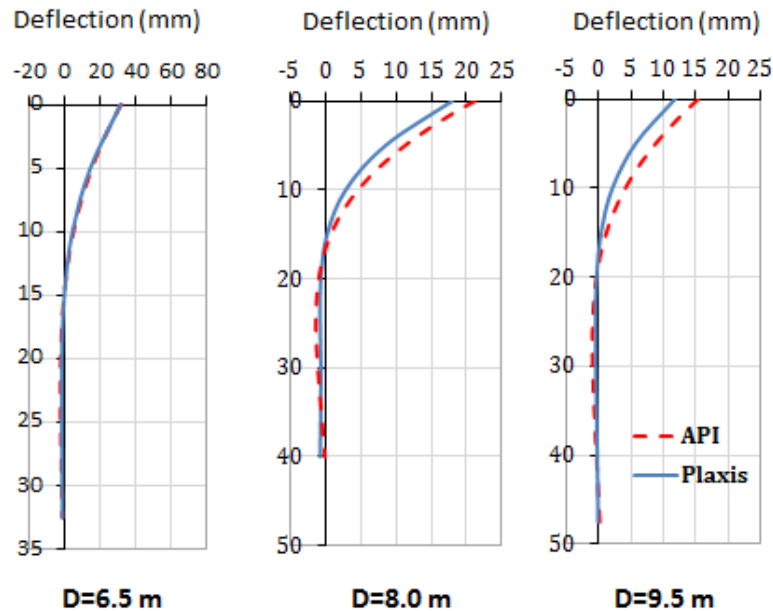
XL Monopile Study

Comparison of XL Monopile design according to API versus novel FEM-based methods

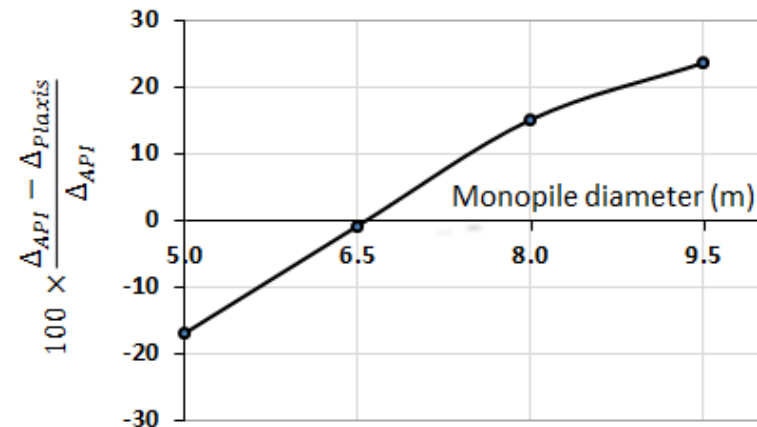
- Numerical modelling of XL monopiles with various diameters under the static loads
- $D = 6.5\text{m}, 8.0\text{m}, 9.5\text{m}$ $L/D = 5.0\text{m}$
- Generic North Sea soil profile
- Modelling monopile geometry and associated loads in Lpile to obtain API results







evaluation of modelling assumption on
the lateral capacity & possible cost savings



The reliability of the API approach depends not only on the monopile diameter, but also on the range of stresses the soil undergoes.

Publication



Attari et al., (2015) Comparative Study of the Design Methods for Large Diameter Offshore Monopiles. The European Wind Energy Association Annual Event 2015

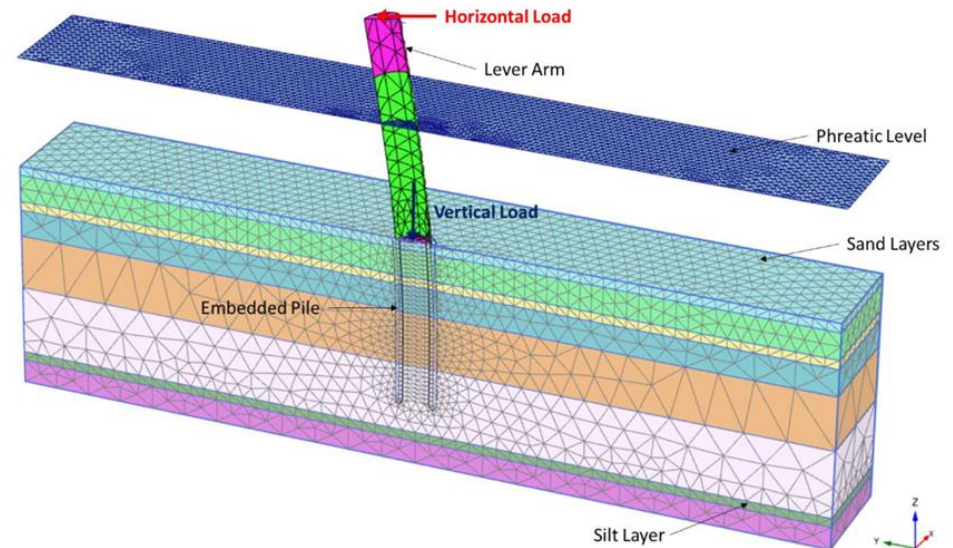
Monopile Design – FLS & DLS case

- Structural fatigue checks - Materials within structure to last beyond specified design life.
 - Fatigue check performed using linearized 'p-y' springs
 - Should use secant 'p-y' stiffness under normal operating loads (Design Equivalent Loads)
 - Need to work very closely with turbine suppliers

- Dynamic checks to ensure natural frequency of structure lies outside exclusion bands,

- Stiffness and Damping are key to dynamics and fatigue

- More efficient design approaches result in
 - Reduction in monopile size
 - Reduction of steel tonnage below mudline
 - Saving money on cost of steel, cost of transport, cost of installation (offshore time)....
 - Significant CAPEX cost reductions

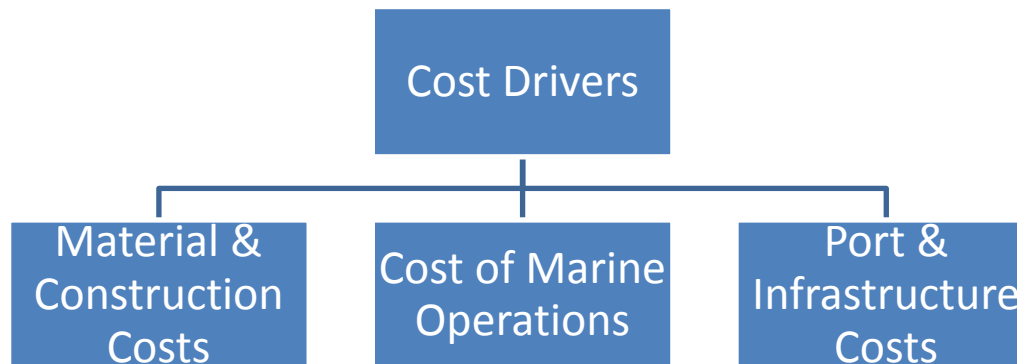
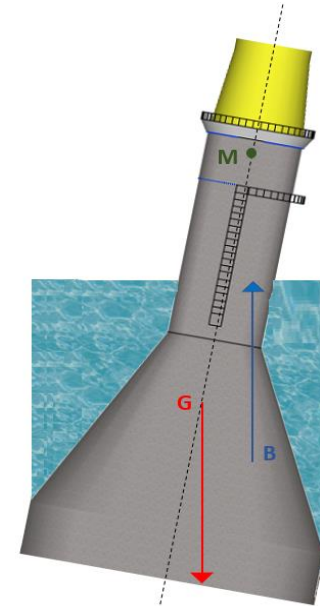
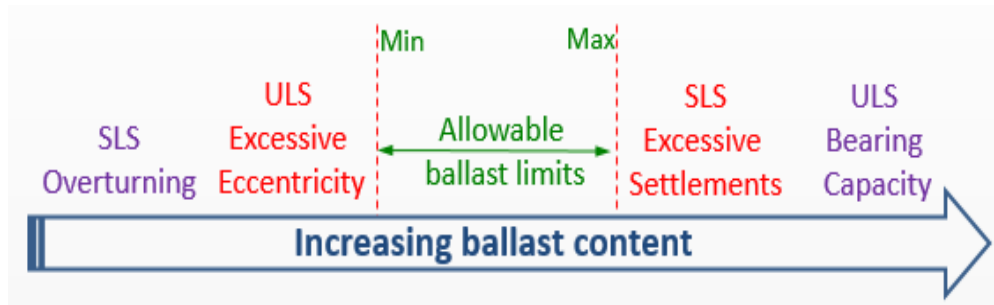


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There are two sides to the design of a GBF:

- Maintaining sufficient stability
- Weight optimisation



Parametric Study of a Self-Buoyant GBF

Objective: Making the structure lighter while maintaining stability

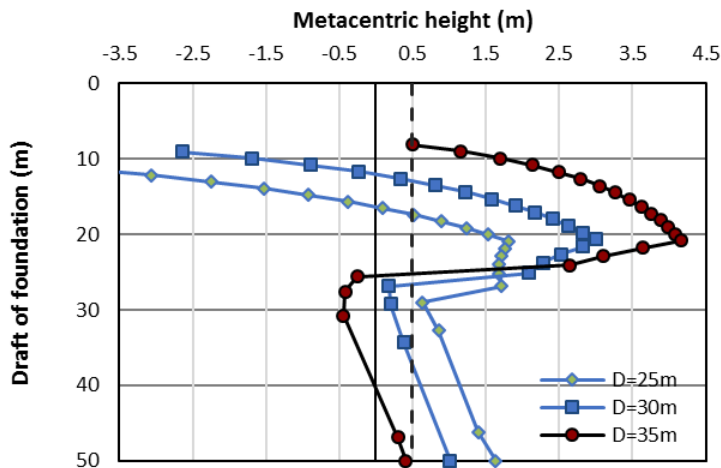
Some of the variables considered included:

- Base diameter
- Height of compartments
- Height of the conical part of foundation
- Ballast mass

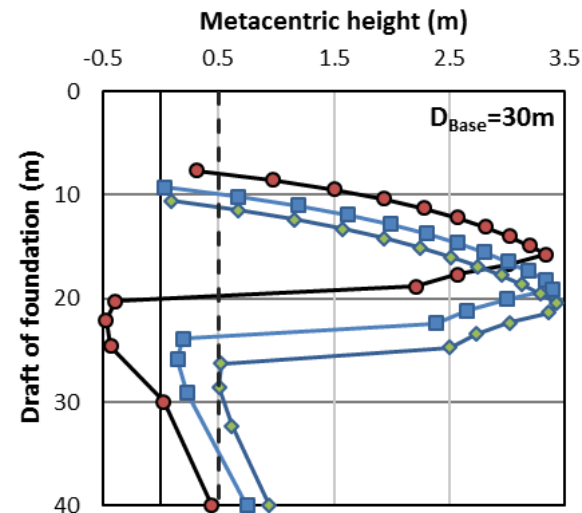
Publication



Attari et al., (2016) "Design Drivers for Buoyant Gravity-based Foundations".
Journal of Wind Energy.

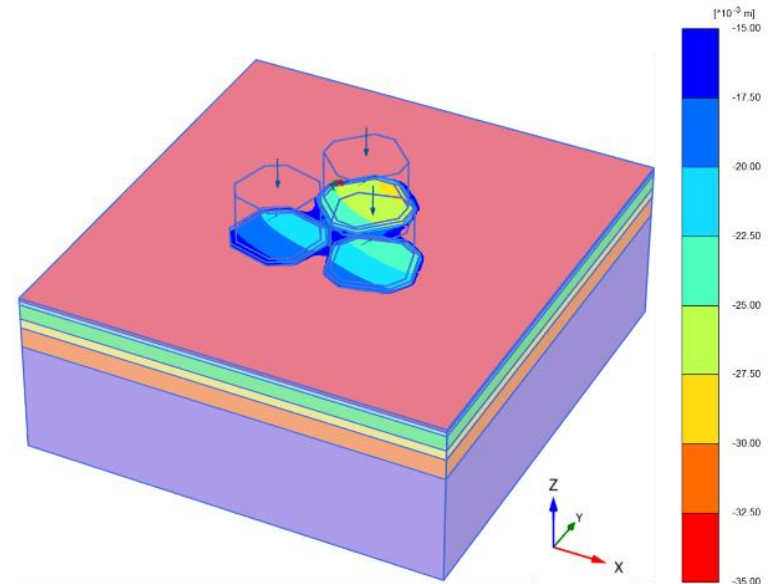
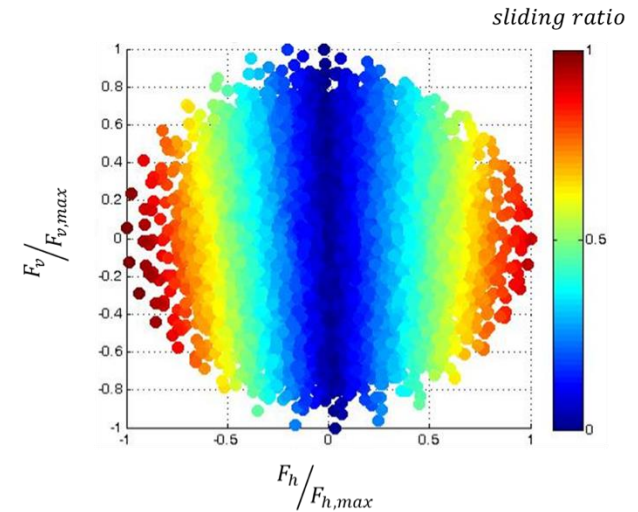
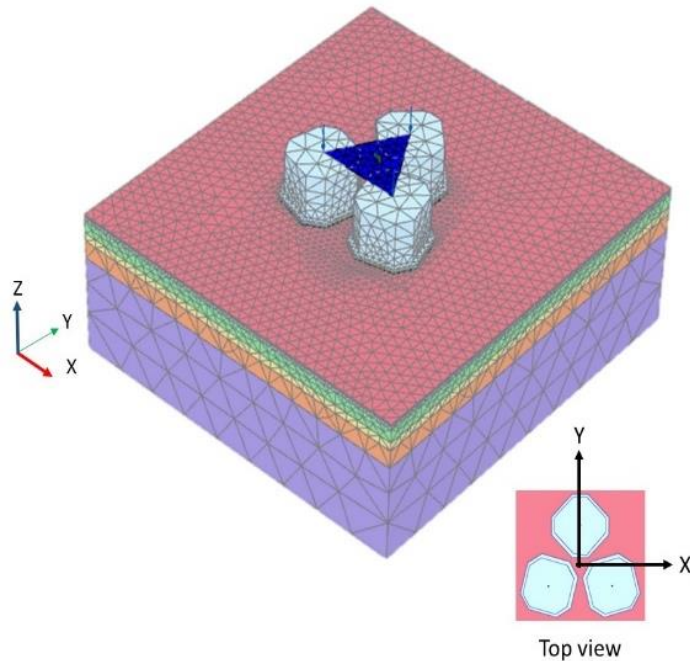


Variation of metacentric height with base diameter during ballasting ($WD=50m$; $H_{cylinder}=20m$; $H_{Cone}=15m$)



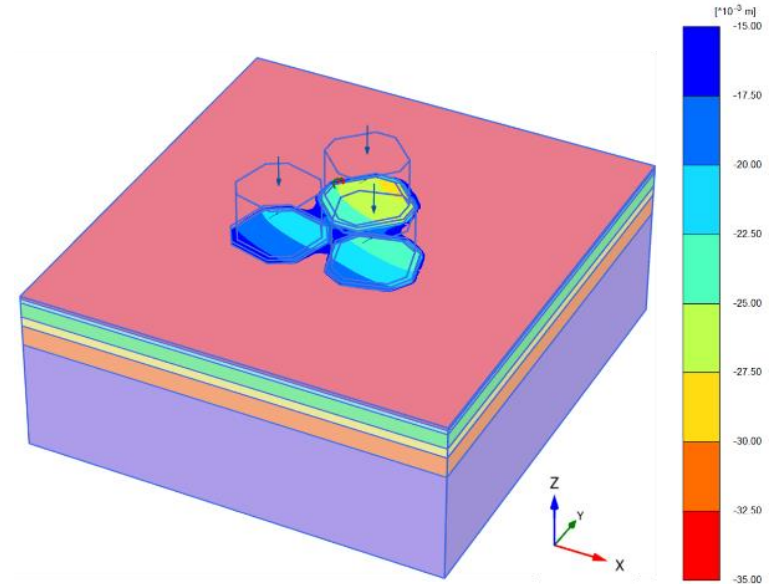
Variation of metacentric height during ballasting at $D_{Base}=30m$ ($WD=40m$; $H_{Cone}=15m$)

- Geotechnical Design of GBFs
- Detailed analysis of cyclic pore pressure response
- Advanced 3D FE analysis and analytical checks



Gravity Base Design

- Bearing Capacity
- Settlement / Differential
- Sliding
 - Change in design guidance DNV (2014)
 - Pre 2014 – $H_d < V_d \cdot \tan(\varphi) < 0.4$
 - Post 2014 - $H_d < r \cdot V_d \cdot \tan(\varphi)$
 - r is roughness parameter which is 1.0 for soil
 - soil or <1 for soil structure



GEOTECHNICAL DESIGN DRIVER – SLIDING !

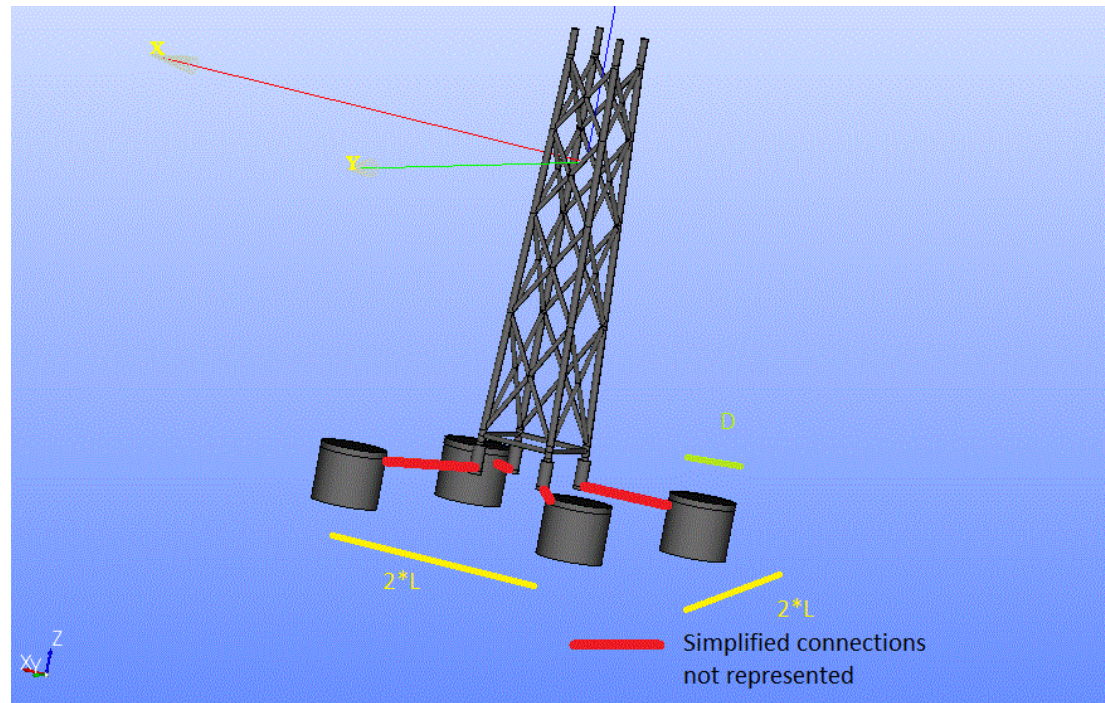
- Researching on geometrical optimisation of these structures has contributed to:
 - Lowering material consumption by designing lighter yet equally stable foundations
 - Savings in manufacturing costs
 - Elimination of expensive jack-up vessels by towing and ballasting gravity based foundations
 - Significant savings in transportation and installation costs

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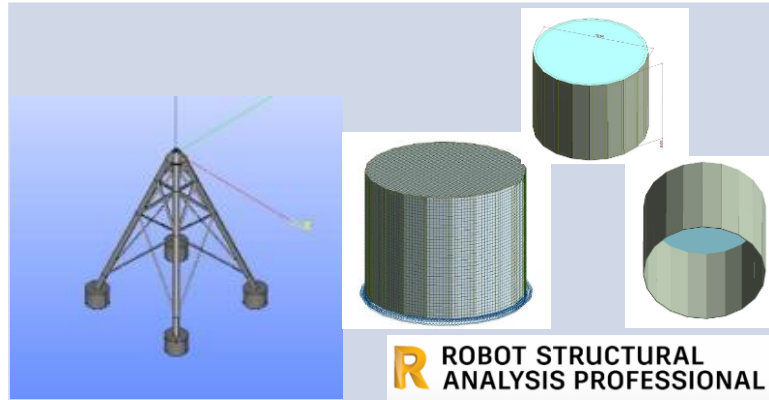
Floating Jacket Design with the Use of Suction Buckets

- Design of a floating jacket
- Design of suction caissons as buoyancy tanks
- Structural rationalisation of the caissons (Geotechnical/structural capacity check of suction buckets)

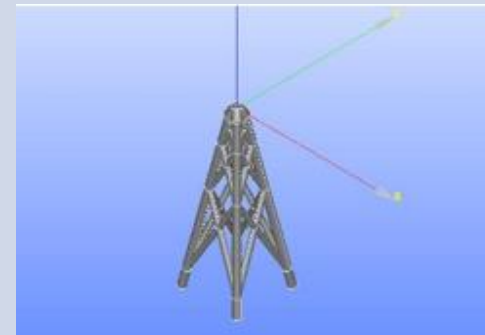


Two sets of design optimisations were done for jacket foundations:

Optimised designs for jackets brought on site floating



Optimised designs for jackets brought on site non-floating



	Jacket brought floating on site	Jacket brought on barge
Jacket Structure Weight	1200 – 1450 Tonnes	1200 – 1800 Tonnes
Foundation Weight	Suction buckets: 420 Tonnes	Not evaluated in the framework of the study
Ballast Weight	300 Tonnes	0
Transportation mean	Tug	Barge & Tug
Installation mean	Vessel, possibly with reduced lifting capacity	Vessel with conventional lifting capacity

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Conclusions

- Offshore Wind Industry undergoing significant expansion over the coming decade
- Costs are rapidly falling as the industry matures and converges on optimum technical solutions and specific design procedures
- The Leanwind design procedures are being applied in industry today.



Thanks for your attention!



Photo credit: Deme Group.